

Membrane curvature controls dynamin polymerization

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The generation of membrane curvature in intracellular traffic involves many proteins that can curve lipid bilayers. Among these, dynamin-like proteins were shown to deform membranes into tubules, and thus far are the only proteins known to mechanically drive membrane fission. Because dynamin forms a helical coat circling a membrane tubule, its polymerization is thought to be responsible for this membrane deformation. Here we show that the force generated by dynamin polymerization, 18 pN, is sufficient to deform membranes yet can still be counteracted by high membrane tension. Importantly, we observe that at low dynamin concentration, polymer nucleation strongly depends on membrane curvature. This suggests that dynamin may be precisely recruited to membrane buds' necks because of their high curvature. To understand this curvature dependence, we developed a theory based on the competition between dynamin polymerization and membrane mechanical deformation. This curvature control of dynamin polymerization is predicted for a specific range of concentrations (~0.1–10 μM), which corresponds to our measurements. More generally, we expect that any protein that binds or self-assembles onto membranes in a curvature-coupled way should behave in a qualitatively similar manner, but with its own specific range of concentration.

force | nucleation | fission | endocytosis | dynamin-like proteins

Membrane remodeling is an essential task of proteins involved in membrane traffic (1, 2). Dynamin is a large GTPase that has been shown to polymerize into a helical collar at the neck of endocytic buds (3), where it subsequently plays a key role in the formation of endocytic vesicles through fission (4–8). This function is fundamental, as the knockout of the dynamin neuronal isoform leads to striking defects in synapse organization and results in a strong dysfunction of neuronal activity (9). The recruitment of dynamin to endocytic buds is thought to depend on the local synthesis of phosphatidylinositol(4,5)bisphosphate (PIP_2), as dynamin has a PIP_2 binding pleckstrin homology (PH) domain (10). Dynamin is recruited late in clathrin-coated vesicle formation, as seen by total internal reflection fluorescence (TIRF) microscopy (11–13). Because PIP_2 is also responsible for the binding of clathrin coats, it is expected to be present at the clathrin bud from the beginning of its formation. Thus, another explanation was suggested: Proteins that interact with dynamin and possess a curvature-sensing Bin-Amphiphysin-Rvs (BAR) domain (such as endophilin and amphiphysin) were proposed to sense the high curvature of the neck and recruit dynamin (14). Because the curvature of the neck is increasing during clathrin-coated vesicle formation to finally reach the range needed for BAR recruitment, this could explain the arrival of dynamin at the very late stage of clathrin-coated vesicle formation. However, in solution, dynamin spontaneously associates into helices and rings (15) with an internal radius of ≈ 10 nm. Dynamin can also polymerize around preformed lipid nanorods of typically 10- to 15-nm radius containing PIP_2 (16) and around microtubules, onto which it was

first purified (17). Binding of dynamin to liposomes has been shown to depend on liposome size (18), and theoretical calculations suggest that dynamin could be recruited by curvature-driven long-range interactions between membrane-bound dimers of dynamin (19). Taken together, these observations may indicate that dynamin polymerizes preferentially along cylindrical structures with a radius close to its spontaneous radius of curvature.

Dynamin was one of the first proteins shown to tubulate protein-free charged liposomes (8). Because the final tubules are circled by dynamin helices (8, 20), it is thought that dynamin polymerization provides the energy needed to deform the liposome membranes into a highly curved tubular structure. Another explanation is that hydrophobic loops present in the PH domain of dynamin (18) could generate spontaneous curvature like the BAR domain structure (21), and that polymerization would just be required to stabilize the tubular shape. To discriminate between these hypotheses, forces and energies involved in polymerization have to be measured.

In this paper, we have measured the polymerization force of dynamin and confirmed that it primarily deforms membranes through a scaffolding mechanism, forcing the membrane to adopt a tubular shape. We also show that the nucleation of the dynamin polymer is controlled by membrane curvature at low concentration. We find that at 440 nM dynamin in solution, spontaneous polymerization of dynamin can be triggered on tubules with radii ranging between 10 and 30 nm, but not on larger tubules. This suggests that the increasing curvature at the neck of closing clathrin-coated pits could per se trigger the polymerization of dynamin. We also provide a mathematical description of this effect that predicts the assembly curvature dependence as a function of dynamin bulk concentration, and show that even if dynamin deforms membranes at high concentration, its polymerization can be controlled by membrane curvature at low concentration.

Results

To measure the force applied by dynamin polymerization onto preformed membrane tubes with an initially imposed radius r_b , we built a microscopy setup (22) that combines a micropipette used for the manipulation of giant unilamellar vesicles (GUVs) and optical tweezers (OT) to extract a membrane tube and measure the force f_b to hold it (Fig. 1). The membrane tension σ

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To confirm that dynamin was polymerized and not simply adsorbed, and to better observe the process of tube coverage, we reduced the dynamin concentration by 30-fold. In the presence of dynamin at 440 nM in solution, small dynamin seeds appeared on the tube and their length steadily increased (Fig. 2D and Movie S3) at an average rate of 14 nm/s (Fig. S3). This nucleation/growth process of dynamin structures confirms a direct polymerization, because adsorption would yield a uniform distribution on the tube. Further confirmation came from fluorescence recovery after photobleaching (FRAP) experiments, as no recovery was observed after bleaching of the dynamin-coated tube (Fig. S4). However, although optically homogeneous, the polymer coat contains discontinuities, as also shown by FRAP (Fig. S5). Even if not detected by our imaging system, the rapid appearance of the seeds suggests that their nucleation is due to dynamin dimers already adsorbed on the membrane that rapidly cluster together on the tube. While these clusters grew, the tube force remained equal to f_b (Fig. 2E, 2–4), but when full coverage was reached, the force dropped to f_d (see Fig. 2E, 5–6). We note that, if adsorption of dynamin to the bare tube significantly affected its spontaneous curvature or bending modulus, we would expect $f \neq f_b$ before full coverage is reached. Hence, our observations confirm that adsorption of dynamin to the bare tube has a negligible effect on the membrane, probably because surface concentration of nonpolymerized dynamin dimers is low, and that before full coating of the tube, the force is imposed by the noncoated sections of the tube. Rather, dynamin polymerization is needed to produce the force required to bend the membrane (SI Mathematical Modeling).

A second important observation is that, at a concentration of 440 nM, dynamin cannot polymerize on tubes that are too wide (i.e., large radii, 50–100 nm; Fig. 2D), and the nucleation of dynamin seeds requires the tube radius to be reduced through increasing the tension (Eq. 1). Only after a small enough radius was reached was polymerization suddenly triggered. Another striking fact is that dynamin was only seen on the tube and not on the GUV (see Fig. 1B). These observations suggest a strong dependence of dynamin polymerization on the curvature of the membrane. To characterize this dependence, we pulled tubes from GUVs held with low aspiration pressure. We then increased the membrane tension in discrete steps, thereby decreasing the tube radius. A typical experiment is shown in Fig. 3A and B (see also Fig. 2D and E and Movie S3), in which several stepwise increases of membrane tension were required before polymerization commenced. Once the radius was sufficiently small, several clusters of dynamin appeared within a few seconds (Fig. 3A and B). For each experiment, tube radii were deduced from Eq. 1 to determine the bounds on the critical radius for dynamin polymerization. For each vesicle, the upper bound was the smallest radius before polymerization started, whereas the lower bound was the radius at which polymerization was observed. Figure 3C shows that the radius intervals for a population of 11 vesicles are spread between 10 and 35 nm, with an average value of 18.5 ± 6 nm. Therefore, we conclude that, at a concentration of 440 nM, dynamin is not able to polymerize on a membrane tube larger than approximately twice its internal diameter.

As dynamin has been described in the past as a curvature-inducing protein at high concentration, we wondered how this curvature-dependent nucleation of dynamin evolved with concentration. Strikingly, our observations suggest that the curvature-dependent nucleation of dynamin and its ability to deform membranes are not independent, as dynamin is still able to squeeze tubes under conditions where its nucleation is curvature-dependent (Fig. S6). To be able to squeeze the tube to 10 nm, dynamin polymerization onto the membrane should generate enough force to overcome the force needed to squeeze the tube more. Obviously, the force needed to squeeze a tube is dependent on its initial radius, large tubes requiring more force to be squeezed to 10 nm

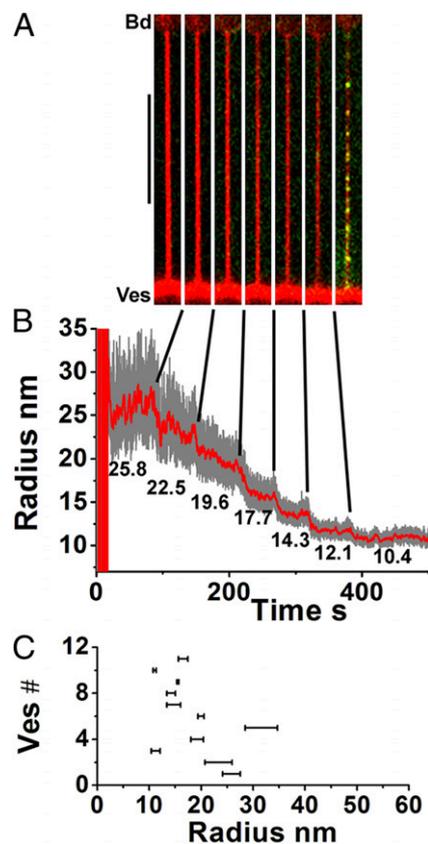


Fig. 3. Curvature control of dynamin nucleation. Images of the membrane tube (A) (membrane, red; dynamin, green) following each stepwise reduction of tube radius (nm) as indicated in B. Polymerization of dynamin is only visible for the smallest tube radius. (Scale bar, 10 μ m.) (C) Critical radius windows obtained from 11 vesicles.

than smaller ones. On the other hand, dynamin polymerization force P depends only on bulk concentration, because it is equivalent to a chemical potential. By comparing these two forces, we have theoretically determined the conditions for dynamin nucleation in terms of concentration and tube radius (SI Mathematical Modeling and Fig. S7). We define conditions where nucleation occurs as values of concentration and radius for which dynamin polymerization force is higher than the force required to squeeze the tube. Here we always consider that dynamin is binding and polymerizing to a preformed tubule, and does not have to form the tubule. Our measurement of P made at 12 μ M allows us to estimate P at any concentration (SI Mathematical Modeling), assuming that the dynamin solution is overall very diluted (much less than 1 M). We can then predict the existence of three regimes as a function of the concentration (Fig. 4):

- (i) For very low dynamin concentrations ($c < c_1^* = 280$ nM or $P < 0$), a tube should always remain uncoated, independent of its initial radius. Indeed, we have checked experimentally that at 50 nM, dynamin is unable to polymerize on the tubule, however small its radius (Fig. 4).
- (ii) For intermediate dynamin concentrations ($c_1^* = 280$ nM $< c < c_2^* = 12.6$ μ M or $0 < P < \pi\kappa/r_d$), we predict that dynamin can polymerize on tubes within a restricted range of radii: $r_c^- \leq r \leq r_c^+$ (see Fig. 4), enclosing dynamin radius value r_d . Thus, if the tube is too thin ($r < r_c^-$) or too thick ($r > r_c^+$), dynamin should not be able to polymerize. As shown in Fig. 4, r_c^+ increases rapidly for concentrations above c_1^* . From the expres-

sion of r_c^+ (see legend of Fig. 4), it is possible to calculate the critical radii for any dynamin concentration, and in particular predict that r_c^+ (440 nM) = 20 nm. This is consistent with the critical radius measured independently above (Fig. 3C). Also, we observe that for 2.5 μ M, dynamin spontaneously polymerizes onto tubules below 30–40 nm, suggesting that the critical radius is around 40 nm, consistent with the value predicted from the theory (see purple line in Fig. 4).

(iii) For high dynamin concentrations ($c > c_2^* = 12.6 \mu$ M or $\pi\kappa/r_d < P$), we predict that dynamin should polymerize on all membrane tubes that have a radius of curvature larger than r_d , including membrane tubes of zero curvature.

Importantly, we describe here two regimes where dynamin behaves first as a curvature sensor (its nucleation being dependent on membrane curvature; see point ii), and a regime where dynamin behaves like a curvature generator (formation of coated tubes is independent of their curvature; see point iii).

Discussion

In the first set of experiments reported above at high dynamin concentration, we have shown that dynamin actually polymerizes on preformed tubes and have measured its polymerization force at this concentration (12 μ M). A first consequence of our experiments is that dynamin polymerization under these conditions generates enough force to deform membranes at low tension ($<10^{-6}$ N/m). Moreover, our experiments show that for membrane tensions superior to 10^{-5} N/m, $f_d > 0$ (Fig. 2C). This means that for tensions that are in the range of typical cellular membrane tensions ($\sim 10^{-5}$ N/m) (31), dynamin should not be

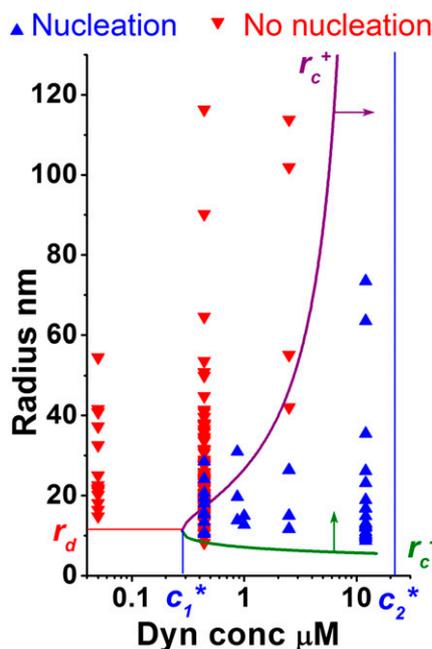


Fig. 4. Phase diagram of dynamin nucleation as a function of tube radius and dynamin concentration. Experimental results are marked with triangles (red, inverted = no nucleation; blue, upright = nucleation). Boundaries of the region of dynamin nucleation, r_c^+ (purple line, arrow) and r_c^- (green line, arrow), were calculated for the theoretical model: $r_c^- = \frac{r_d}{1 + \sqrt{Pr_d/\pi\kappa}} > r_d$ and $r_c^+ = \frac{r_d}{1 + \sqrt{Pr_d/\pi\kappa}} > r_d$ (SI Mathematical Modeling). Nucleation should not occur below the lower concentration, c_1^* . Above the higher concentration, c_2^* , nucleation should always occur, independent of membrane tube radius. r_d corresponds to the internal radius of a dynamin-coated membrane tube.

able to deform membranes into tubules, as its polymerization force can be overcome by high membrane tension. This supports the idea that recruitment of proteins to the membrane can be controlled by tuning cellular membrane tension, and could explain how endocytosis is up-regulated when plasma membrane tension is reduced (32).

Our second set of data shows that dynamin nucleation is strongly dependent on membrane curvature at low concentrations. This may reflect the ability of curved dynamin oligomers to preferentially polymerize on curved areas of the membrane. Moreover, the curvature-dependent nucleation of dynamin is highly concentration-dependent. More generally, any protein that interacts with membranes in a curvature-coupled manner should have the same type of concentration-dependent behavior. It can be understood in terms of the interplay between membrane curvature and chemical equilibrium between membrane-bound and -unbound forms of the protein. At low concentration the protein is mostly unbound, but preferentially binds onto curved parts of the membrane. At high bulk concentration, chemical equilibrium is displaced toward the bound form, in turn forcing the membrane to curve, as a protein-coated membrane is more stable when curved. In previous studies, the abilities of proteins to sense membrane curvature or to curve membranes have sometimes been regarded as separate functions. Our study suggests that these two functions should be effective for any protein interacting with membranes in a curvature-coupled manner. Importantly, for each protein, a specific range of concentrations (given by its specific concentrations c_1^* and c_2^*) should exist, separating conditions where the protein acts more as a curvature sensor or more as a curvature inducer. We predict that the specific physico-chemistry of membrane-protein interactions that have been described to explain curvature-sensing versus curvature-inducing functions (33, 34) will have a strong influence on the (c_1^* , c_2^*) values. To discriminate the function of a protein in vivo, one must compare its physiological concentration with its specific critical concentrations c_1^* and c_2^* . For dynamin, we found that the concentration range thought to be physiological (4) lies between c_1^* (a few hundred nM) and c_2^* (a few tens μ M) and, consequently, dynamin nucleation could be regulated by membrane curvature in vivo. Our findings suggest that dynamin could be recruited to the neck of closing clathrin-coated pits when their curvature is sufficiently high, and that its polymerization further constricts them to 10 nm. In vivo, dynamin appears at the clathrin-coated pits at the end of their formation (11–13), when the neck has a radius of ~ 20 nm (35), close to the value of the critical radius (19 nm) we found for dynamin at 440 nM.

Materials and Methods

Materials. Egg L- α -phosphatidylcholine (EPC), 1,2-distearoyl-sn-glycero-3-phosphoethanolamine-N-[biotinyl(polyethyleneglycol)2000] [DSPE-PEG(2000)biotin] and brain L- α -phosphatidylinositol(4,5)bisphosphate [PtdIns(4,5)P₂] were obtained from Avanti Polar Lipids. Red fluorescent GloPIPs BODIPY TMR-PtdIns(4,5)P₂-C₁₆ (GloPIP₂) was obtained from Echelon Biosciences.

Giant Unilamellar Vesicles. Giant unilamellar vesicles were formed using a slightly adapted version of the electroformation method (36, 37). A mixture of 30 μ L CHCl₃, 2.25 μ L EPC (10 mg/mL), 1 μ L PtdIns(4,5)P₂ (5 mg/mL), 1 μ L of GloPIP₂ (0.25 mg/mL), and 0.4 μ L DSPE-PEG(2000)biotin (10^{-2} mg/mL) was made. This mixture was vortexed, heated to 50 $^{\circ}$ C, and spread on two indium titanium oxide (ITO)-coated glass slides with a Hamilton syringe in an oven at 50 $^{\circ}$ C to prevent demixing of the lipids and ensure a homogeneous distribution of PIP₂. The lipid deposits were further dried by leaving the slides 1 h at 50 $^{\circ}$ C. Next, a growth chamber was built using the ITO slides, which were separated by Teflon spacers and sealed with Vitrex wax (37). The chamber was then filled with a sucrose solution at 213 mOsm, osmotically equilibrated with the experimental GTPase buffer [20 mM Hepes (pH 7.4), 100 mM NaCl, 1 mM MgCl₂]. An AC field (10 Hz, 1.1 V) was then applied for 2 h while keeping the chamber at 50 $^{\circ}$ C.

Dynamin Purification. Dynamin was purified from rat brains using the GST-tagged SH3 domain of rat amphiphysin 1 as an affinity ligand as previously described (6, 16). Briefly, six brains were homogenized with a 60-mL dounce in buffer A [20 mM Hepes (pH 7.4), 150 mM NaCl, 1 mM EGTA, 1 mM DTT, 1% Triton X-100] and centrifuged at 40 krpm in a Ti70 rotor (Beckman), and the supernatant was incubated for 2 h with glutathione beads to which 3–5 mg of SH3 domain of amphiphysin was attached. Next, the beads were batch-washed several times. Elution was done with high salt [20 mM Hepes (pH 7.4), 1.2 M NaCl, 1 mM MgCl₂]. Unlabeled dynamin was dialyzed against storage buffer [20 mM Hepes (pH 7.4), 100 mM NaCl, 1 mM MgCl₂], concentrated using Amicon devices (50 kDa CO), aliquoted, flash-frozen in liquid N₂, and stored at –80 °C.

To fluorescently label dynamin, we dialyzed dynamin against PBS, 50% glycerol. The labeling reaction was conducted using standard procedures (Alexa-488 protein-labeling kit from Invitrogen). Fluorescently labeled protein was further dialyzed (2–3 h) against storage buffer, concentrated, aliquoted, flash-frozen in liquid N₂, and stored at –80 °C.

Experimental Setup. The setup was based on a commercial Nikon TE2000 inverted microscope modified with the optional stage riser (Nikon) to create an extra port (22). The confocal head was the eC1 confocal system (Nikon) with two laser lines ($\lambda = 488$ nm; $\lambda = 543$ nm).

The micropipette technique has already been described (38), and was used for setting GUV tension. Pipette manipulation was achieved with a homemade micromanipulator clamped on the microscope. In our experiments, a micropipette of about 3- to 4 μ m diameter at the tip was connected to a mobile water reservoir, which allowed control of the membrane tension of the GUV from 5.10^{-6} to 2.10^{-4} N·m⁻¹.

To create a single, non-moving optical trap, light from an ytterbium fiber laser (1070 nm, 5 W, continuous wave; IPG GmbH) was injected into a 100 \times /1.3 NA oil immersion objective (Nikon) using a heat-reflecting mirror ($\lambda_c = 900$ nm; Melles Griot). The x-y-z position of the trap was set with external optics in a configuration similar to that in ref. 24. The position of the polystyrene bead in the trap was recorded and analyzed off-line using custom-made video-tracking software (Konstantin Zeldovitch, Paris, France) with a temporal resolution of 40 ms and a subpixel spatial resolution of 35 nm. The trap stiffness was calibrated using the Stokes drag force method (39). The stiffness of the tweezers was found to be 450 ± 30 pN·nm⁻¹·W⁻¹.

Bright field imaging was done using a fluorescence illumination arm as an imaging port. To do so, the fluorescence filter cube was replaced by a heat-

reflecting mirror ($\lambda_c = 750$ nm; PGO GmbH Iserlohn) and a convergent lens was added to the fluorescence excitation path to project the field diaphragm plane on a video camera. The video signal was then digitized using Labview-based custom software. To avoid overlap between bright field and confocal data, only near-infrared light was used for bright field illumination. This was achieved by inserting a bandpass filter (750–900 nm; visible light absorbing RG9 Schott glass) in front of the bright field illumination halogen lamp of the microscope.

Sample Preparation. Three to four microliters of streptavidin-coated polystyrene beads of 3.2- μ m diameter diluted 20 times (Spherotech) were mixed with 200 μ L GTPase buffer and 2–5 μ L of GUVs taken directly from the growth chamber. In experiments with dynamin in bulk, unlabeled dynamin and fluorescent dynamin (10–20% mol/mol) were added to this solution to obtain the appropriate concentration. This solution was inserted into the sample chamber which was previously incubated with 4 mg/mL casein in GTPase buffer for 5 min.

In experiments in which a second micropipette was used for local dynamin injection, a 10- to 12 μ m-wide pipette was filled with 3–5 μ L dynamin solution by capillary. Then, the dynamin solution was pushed toward the tip of the pipette by connecting it to an Eppendorf Femtojet microinjector and applying high pressure (100–300 mPa). Once the solution reached the tip, the pressure was reduced to its minimum (15 mPa) and the pipette was inserted into the chamber. The pipette was kept at a continuous flow, and the pipette was moved into the observation field to perform local injections of dynamin.

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Supporting Information

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Mathematical Modeling

Here we discuss in detail the assumptions underlying the theoretical considerations presented in the main text. An effort is made toward an untechnical, yet rigorous, treatment. First we introduce our model, and then four specific points are discussed.

Presentation of the Model. We consider a membrane tube pulled by optical tweezers and connected to a membrane tension reservoir (the aspiration-controlled vesicle). The tube has a length L and is partially covered by a possibly discontinuous coat of dynamin over a total length L_d . We neglect the transition regions between bare and dynamin-covered sections of the tube. Taking into account a force f externally applied on the tube (by the optical tweezers), we write the free energy of the system as the sum of the free energies of the two types of regions, plus the work of the force:

$$F = \mu_b(L - L_d) + \mu_d L_d - fL, \quad [S1]$$

where μ_b and μ_d stand for the free energy per unit length of the bare region and the dynamin-covered region, respectively. For μ_b we use the classic expression (1)

$$\mu_b = \frac{\pi\kappa}{r} + 2\pi r\sigma, \quad [S2]$$

where κ is the bending modulus of the cylindrical membrane, r is its radius, and σ is its surface tension. We consider timescales that are large compared with the mechanical equilibration of the tube and the equilibration of the lipids with the reservoir (≈ 1 s). Therefore, we assume in all of the following that the bare sections minimize their free energy with respect to r and that σ is equal to the value imposed by the reservoir. This yields

$$r = \sqrt{\frac{\kappa}{2\sigma}}, \quad \mu_b = 2\pi\sqrt{2\sigma\kappa}. \quad [S3]$$

To construct the free energy of the dynamin-covered part, we take into account the bending and tension energies of the membrane as well as a dynamin-related term P . This term accounts for the free energy difference between dynamin in solution and in the membrane-bound polymerized state. This includes the following effects:

- The binding energy of a dynamin dimer to an already existing helix—this quantity might depend on the salinity of the solution.
- The energy gain of dynamin upon binding the membrane, and the change of the membrane energy upon dynamin binding [e.g., insertion of dynamin's hydrophobic loops into the bilayer (2)]—this quantity depends on the chemical composition of the membrane.
- The loss of entropy for leaving the solution and going into the immobilized polymerized state—this quantity depends on the concentration c of the dynamin solution.
- The elastic cost of deforming the helix away from its preferred radius—this quantity depends on the inner radius r_d of the dynamin helix.

The free energy per unit length of the dynamin-covered tube then reads

$$\mu_d = \frac{\pi\kappa}{r_d} + 2\pi r_d\sigma - P(c, r_d), \quad [S4]$$

where $P > 0$ denotes a situation where dynamin dimers are more stable in the polymerized state than in solution.

Throughout this work, we do not consider the dependence of P on r_d , and write $P(c)$. This assumption is justified theoretically in *SI Section 1*, where we argue a priori that dynamin is so stiff that the radius r_d is not influenced by membrane tension. This makes the r_d dependence of P irrelevant. This point is demonstrated experimentally in the main text. In *SI Section 2*, we prove that thermodynamic stability implies that forming a dynamin helix is only possible in a certain (c -dependent) range of membrane tensions, which according to Eq. S3 can be translated into a certain range of initial tubule radii. In *SI Section 3*, we show that under mechanical and membrane equilibrium conditions, the force exerted by the tube on the optical tweezers is $f_b = \mu_b$ as long as the tube is not fully covered by dynamin ($L_d < L$) and drops to $f_d = \mu_d$ when full coverage is achieved ($L_d = L$).

1. A Priori Argument for a Constant Dynamin Radius

We argue here that the radius of the dynamin helices described in the main text does not depend on the tension of the membrane. Electron microscopy data point in that direction, as they consistently show that dynamin on soft membrane templates has a radius in the vicinity of 10 nm (3–6). However, one could argue that all these references use floppy membrane templates and that the higher membrane tensions used in our experiments might exert stronger stresses on dynamin, therefore deforming it substantially.

The argument given here is a comparison of the elasticities of the membrane and the dynamin helix. The elasticity of the membrane is known to be well-described by its bending modulus $\kappa = 16.1 k_B T$ (see main text). To our knowledge, the only data available in the literature concerning the elasticity of dynamin are a measurement of the persistence length of dynamin-covered tubules performed in ref. 7, which yields $\ell_p = 37.3 \pm 4.6 \mu\text{m}$. We recall that the persistence length is the length over which an elastic filament is curved by the thermal fluctuations of the surrounding medium. It therefore characterizes how difficult it is to bend the filament (a stiff filament will have a large ℓ_p). It is possible to use this value to evaluate the bending rigidity of the dynamin coat. A detailed derivation of this bending stiffness for a particular toy model of dynamin elasticity is proposed in appendix C of ref. 8 and commented on in section IV.B of the same paper. Here we propose an order-of-magnitude argument leading to the same conclusions. We need to compare two quantities:

- On the one hand the elasticity of the dynamin helix, characterized by the elastic constant $k_B T \ell_p \approx 2 \times 10^{-25}$ J.m, which quantifies to what extent the dynamin coat wants to be curved to its preferred radius r_d , assuming the elastic properties of the helix are reasonably isotropic.
- On the other hand the bending modulus κ of the membrane, which quantifies how much the membrane wants to be flat.

Because the former is an energy \times length and the latter an energy, we need to introduce a characteristic length scale of the system to compare them. The appropriate length is obviously the radius of the tube $r_d \approx 10^{-8}$ m. Therefore, we can define the dimensionless ratio characterizing the relative stiffness of the membrane and the helix:

$$\frac{\text{stiffness of the membrane}}{\text{stiffness of the helix}} \approx \frac{\kappa}{k_B T \ell_p / r_d} \approx 3 \times 10^{-3}. \quad [\text{S5}]$$

Because this ratio is much smaller than one, we conclude that the influence of the elastic stresses exerted by the membrane on the helix will be small, and therefore that the radius r_d of the dynamin coat will not be substantially influenced by the membrane, justifying that we consider it constant throughout this work. This assumption is verified experimentally in Fig. 2C, where it is found that $f_d = \mu_d$ depends linearly on σ , which according to Eq. S4 shows that r_d is constant.

2. Threshold Radii and Concentration Regimes

Here we present a thermodynamic criterion for the stability of the dynamin polymer. At equilibrium, we expect that the tube will either be dynamin-coated or bare depending on which situation has the lowest free energy. Therefore, we expect that no nucleation of dynamin oligomers will be observed if a bare tube is the preferred state for a large system.

It is fairly obvious that the polymer stability criterion we are looking for is $\mu_d < \mu_b$ (for instance, one can consider whether minimizing F with respect to L_d yields $L_d = 0$ or $L_d = L$). Using Eq. S2 and S4, it is seen to be equivalent to

$$\sigma - \frac{\sqrt{2\kappa}}{r_d} \sqrt{\sigma} + \left(\frac{\kappa}{2r_d^2} - \frac{P}{2\pi r_d} \right) < 0, \quad [\text{S6}]$$

which with the help of Eq. S3 can be expressed as a condition on the initial bare tube radius r :

$$1 - 2\frac{r}{r_d} + \left(1 - \frac{Pr_d}{\pi\kappa} \right) \left(\frac{r}{r_d} \right)^2 < 0. \quad [\text{S7}]$$

This criterion is illustrated in Fig. S7.

There are three regimes for this inequality, as pictured in Fig. 4D:

- (i) For $P < P_1 = 0$, Eq. S7 has no solution.
- (ii) For $P_1 < P < P_2 = \pi\kappa/r_d$, Eq. S7 is satisfied on the interval

$$r_c^- = \frac{r_d}{1 + \sqrt{\frac{Pr_d}{\pi\kappa}}} < r < r_c^+ = \frac{r_d}{1 - \sqrt{\frac{Pr_d}{\pi\kappa}}}. \quad [\text{S8}]$$

- (iii) For $P_2 < P$, the upper threshold radius diverges and Eq. S7 is equivalent to $r > r_c^-$.

To express r_c^- and r_c^+ as functions of c , we have to specify a particular form for the dependence of P on c . In the limit of a very dilute solution, one can use the ideal solution hypothesis

$$P(c) = P \left(12 \mu\text{M} \right) + \frac{k_B T}{a} \ln \left(\frac{c}{12 \mu\text{M}} \right), \quad [\text{S9}]$$

where $a = 0.85$ nm is the length increment of the polymer upon binding of a dynamin dimer and where the value of $P(12 \mu\text{M})$ is deduced from the measurement of $f_d(12 \mu\text{M})$ (see main text). Eq. S9 allows us to express the boundaries c_1^* and c_2^* of the three concentration regimes described in the main text as the concentrations at which $P = P_1$ and $P = P_2$, respectively. This yields

$$c_1^* = \left(12 \mu\text{M} \right) \times \exp \left[-a \frac{P(12 \mu\text{M})}{k_B T} \right] \approx 280 \text{ nM}, \quad [\text{S10}]$$

$$c_2^* = \left(12 \mu\text{M} \right) \times \exp \left[a \frac{(\pi\kappa/r_d) - P(12 \mu\text{M})}{k_B T} \right] \approx 12.6 \mu\text{M}. \quad [\text{S11}]$$

Finally, we note that the argument presented here concerns equilibrium situations, but that kinetic effects could prevent the observation of dynamin nucleation even at concentrations and tensions where it is favored.

3. Force Drop and the Influence of Dynamin Adsorption

3.1. Tubes Partially Covered by Dynamin. Here we are interested in time scales that are large compared with the mechanical and membrane equilibration times, but short compared with the dynamin growth times. In this section, we therefore consider the growth process of dynamin to be essentially frozen, with L_d fixed. The behavior of the tube on longer time scales is described in *SI Section 3.3*. The partial equilibrium of the system is described by a minimization of F with respect to L and r , but with $L_d < L$ imposed. This yields the force needed to hold the partially dynamin-covered tube:

$$f = \mu_b = 2\pi\sqrt{2\sigma\kappa}, \quad [\text{S12}]$$

which is equal to the force f_b needed to hold a completely bare membrane tube. Hence, a partial dynamin coat does not change the force needed to pull a tube. An intuitive way of seeing this result is to say that although dynamin is able to exert a force while polymerizing, this force can only be visualized in our setup if it pushes the bead held by the optical tweezers away from its resting position. As long as the dynamin helix touches only the bead or only the vesicle or is discontinuous between the two, it will not be able to induce such a displacement, whereas it will if it is continuous. Because the membrane is a two-dimensional liquid on the timescales considered, this situation is exactly that of a swimmer who is unable to move a rock sitting in the middle of the pool, but who will be able to take two rocks apart by placing himself between them and pushing on both of them at the same time.

3.2. Adsorbed Dynamin Has a Negligible Influence on the Tube. In our model, we consider only the influence of polymerized dynamin and not of adsorbed dynamin. Here we show that the amount of dynamin adsorbed on the membrane tube is not only too low to be seen in fluorescence microscopy but also too low to have any measurable mechanical effect. Indeed, in general, proteins adsorbed on a membrane are expected to change its bending rigidity from κ to $\tilde{\kappa}$ and to induce a spontaneous curvature r_0 . Such modifications are expected to change the force needed to maintain a bare tube to

$$\tilde{f}_b = 2\pi\sqrt{2\sigma\tilde{\kappa}} \left(\sqrt{1 + \frac{\tilde{\kappa}}{2\sigma r_0^2}} - \sqrt{\frac{\tilde{\kappa}}{2\sigma r_0^2}} \right). \quad [\text{S13}]$$

Similar to what was discussed above, this result is expected to still be valid if the tube is partially coated by dynamin.

Experimentally, such deviations of the force are not observed. Indeed, we see in Fig. 2E that the force needed to hold the tube does not change upon dynamin injection until the tube is fully covered by the polymer. Hence, we can safely neglect dynamin adsorption.

3.3. Tubes Fully Covered by Dynamin. Here we deal with long time scales, where the dynamin polymer fully covers the membrane tube. This is equivalent to assuming a chemical equilibrium between polymerized dynamin and the dynamin solution. When dynamin fully covers the tube ($L_d = L$), the growing polymer touches both the vesicle and the optical tweezers' bead, hence exerting a force pushing them apart in the same way that a polymerizing microtubule held at one end can exert a force on a wall at its other end (9). Returning to our formalism, we note that $P(c)$ has units of a force, and it can be seen as the force one needs to exert on a polymerizing dynamin helix to stall its growth. This force is exactly equivalent to the stall force of polymerizing microtubules.

In the cases considered in this paper, this force helps the optical tweezers to hold the membrane tube. To prove this, we minimize F with respect to L while imposing $L_d = L$. Assuming that we are in a regime where dynamin polymerizes ($\mu_d < \mu_b$), this is equivalent to minimizing F with respect to r , L_d , and L at the same time. Both procedures yield the force needed to hold a completely coated tube:

$$f_d = \mu_d = \frac{\pi\kappa}{r_d} + 2\pi r_d \sigma - P(c), \quad [\text{S14}]$$

which is clearly the force needed to pull a membrane tube of radius r_d from the vesicle minus the dynamin stall force.

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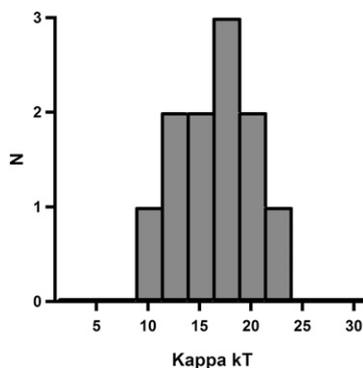


Fig. S1. Histogram of the membrane rigidities κ measured for 11 giant unilamellar vesicles (GUVs) of egg phosphatidylcholine (EPC) + 12.5% PtdIns(4,5)P₂ + 1% GloPIP₂ determined as in ref. 1. The average value is 16.1 $k_B T$.

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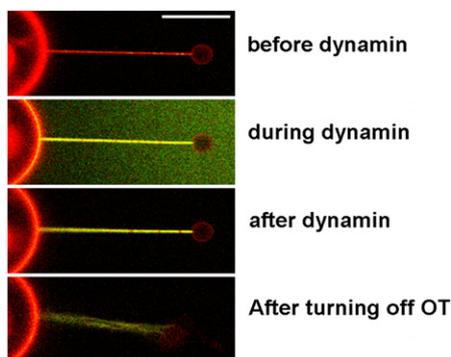


Fig. S2. Stabilization of a membrane tube by dynamin. Dynamin (green) was injected on a tube extracted from a GUV (red) with a bead maintained with optical tweezers (OT). After dynamin injection, the tube was covered with dynamin and the GUV was then moved to a field without dynamin in solution. When the OT was turned off, the tube did not fully retract, and instead just started to move with Brownian motion. (Scale bar, 10 μm .)

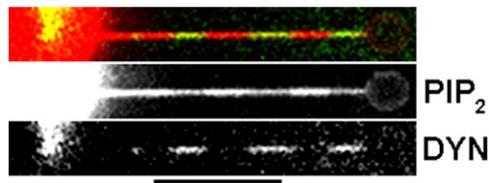


Fig. S6. Squeezing of a membrane tubule by dynamin polymerization. Under appropriate conditions (low fluorescence excitation), it is possible to see a narrowing of the tube (red fluorescence) reflected by a lower fluorescence intensity, where dynamin is polymerized (green channel). (Scale bar, 10 μm .)

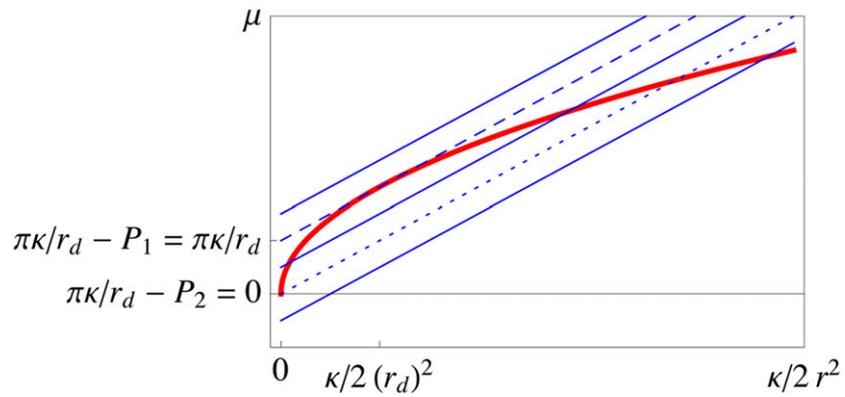
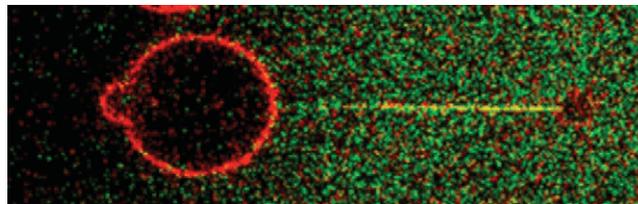
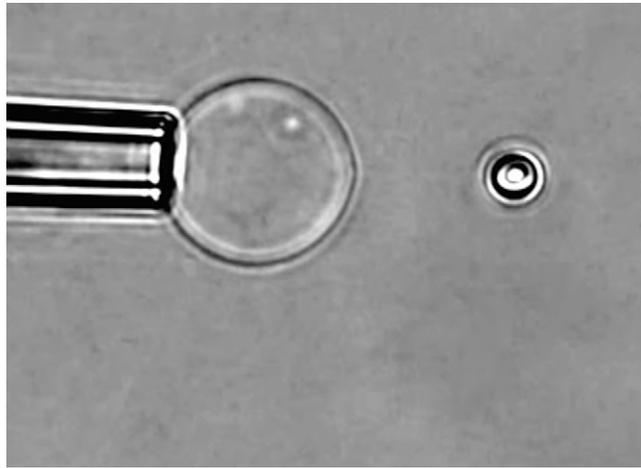


Fig. S7. Plot of the free energies per unit length of the bare tube μ_b (thick red line) and of the coated tube μ_d (blue lines) as a function of $\kappa/2r^2$. The various blue curves are plotted for different values of P . The lower the curve, the larger the P . The parameter regimes where the blue curve lies below the red curve represent situations where dynamin polymerization is energetically favored. We note two changes of behavior as P is varied: For low values of P , the bare tube is always more stable (upper solid blue line); for intermediate values of P , the coated tube is more stable only for intermediate tensions (middle solid blue line); and for large values of P , the coated tubes are always more stable at low tensions, but not at high tensions (lower solid blue line). The value of P_1 limiting the two first regimes is indicated by the dashed blue line, and the value of P_2 limiting the two last regimes is indicated by the dotted blue line.



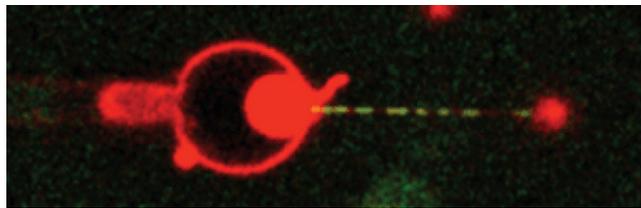
Movie S1. Using optical tweezers, a tube is extracted from a GUV. Then, a second micropipette filled with a 12 μM green-labeled dynamin solution is brought close to the tube. The tube is then rapidly covered with dynamin. See also Fig. 2A.

[Movie S1](#)



Movie S2. DivX codec is needed to read this file. A bead held in optical tweezers is used to pull a tube from a giant vesicle. First, a connection is established between bead and vesicle before the tube is then pulled. In the absence of dynamin, the tube is readily reincorporated after the tweezers are switched off. Next, a tube is again pulled with the optical tweezers and dynamin is injected through a second micropipette. The tweezers are then switched off again, but the tube does not retract fully.

[Movie S2](#)



Movie S3. Movie of data presented in Fig. 2D.

[Movie S3](#)