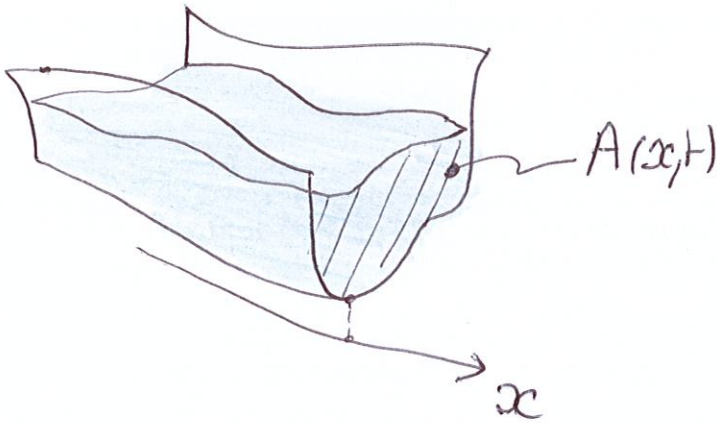


Flood waves

FW 1



conservation equation:

$$\frac{d}{dt} \int_{x_1}^{x_2} A(x,t) dx + Q(x_1,t) - Q(x_2,t) = 0$$

hence $A_t + Q_x = 0$

where Q = flux in m^3/s .

Actually, on real grounds one could add a source term =

$A_t + Q_x = M$

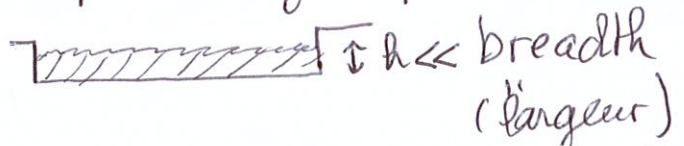
where M represents the supply to the river due to infiltration seepage and overland flow from the catchment.

can one try to write a law $Q = Q(A)$? Let's define the average velocity $V = Q/A$. A slice of thickness dx is subjected to two forces = friction on the bottom and gravity.

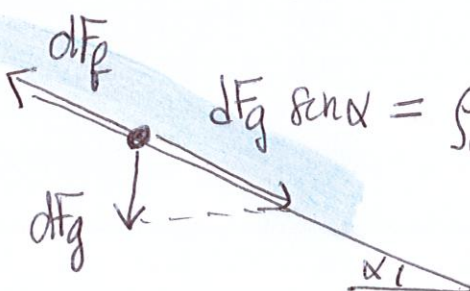
$dF_f \propto V^2, P \text{ and } dx$

and not V as in high school or in Stokes flow = here V^2 is more realistic

wetted perimeter = $\propto A^{1/2}$ for circular cross-section and also independent of A for broad river:



slope α :



$dF_g \sin \alpha = \rho_0 g A dx \sin \alpha$ (ρ_0 = max density of water)

at quasi-equilibrium dF_p and $dF_g \sin \alpha$ should equilibrate (if this hypothesis is violated, no steady flow is possible!) | FW2

writing $dF_p = C_f \rho_0 P V^2 dx$ yields then:

$$\begin{cases} V = \sqrt{\frac{g A \sin \alpha}{C_f P}} \\ Q = VA = \sqrt{\frac{A^3}{P} \frac{g \sin \alpha}{C_f}} \end{cases}$$

this yields $Q \propto A^{3/2}$ or $A^{5/4}$ for broad or circular river
assuming C_f and α constant

Other empirical laws give different power law dependences.

We will assume that

$$Q = C \frac{A^{m+1}}{m+1}$$

where C is a constant and $m > 0$ (also $C \neq 0$)

then the eq. becomes:

$$A_t + (dQ/dA) A_x = M \quad \text{with} \quad dQ/dA = C \cdot A^m$$

this can be nondimensionalized by defining $A = C^{-1/m} \mathcal{A}$

then $C A^m = \mathcal{A}^m$

$$M = C^{-1/m} \mathcal{M}$$

and the eq. becomes: $\mathcal{A}_t + \mathcal{A}^m \mathcal{A}_x = \mathcal{M}$

the simplest assumption is to take $\mathcal{M} = 0$. Slightly better = $\mathcal{M} = C \frac{dA}{dt}$.

In this case, define $a(t) = A(x(t), t) =$ along a characteristics

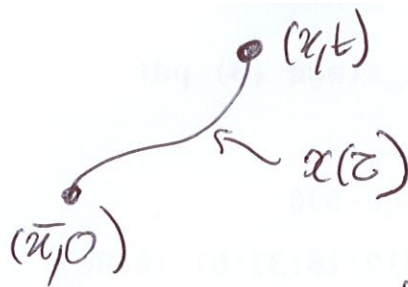
$$\frac{dx}{dt} = A^m \quad \text{one has} \quad \frac{da}{dt} = \mathcal{M}$$

this means that $a(t) = \mathcal{M}t + a(0)$, ie

$A(x, t) = \mathcal{M}t + A(\bar{x}, 0)$ where $(\bar{x}, 0)$ is the starting point of the characteristics which reaches (x, t)

and whose eq. is $\frac{dx}{dt} = A^m = (\mathcal{M}t + \underbrace{A(\bar{x}, 0)}_{A_0(\bar{x})})^m$

along the characteristics:



with $\frac{dx}{dz} = [cVz + A_0(x)]^m \Rightarrow x(z) = \frac{[cVz + A_0(x)]^{m+1}}{cV(m+1)} + C_{ste}$

and then, at time $z = t$:
 (determined by imposing $x(0) = \bar{x}$)

$$x = \frac{[cVt + A_0(x)]^{m+1}}{cV(m+1)} + \bar{x} - \frac{[A_0(x)]^{m+1}}{cV(m+1)}$$

this eq. defines \bar{x} implicitly as a function of x and t

then, one gets $A(x, t)$ by writing:

$$A(x, t) = cVt + A_0(x) = cVt + A_0 \left(x - \frac{[cVt + A_0(x)]^{m+1}}{cV(m+1)} + \frac{[A_0(x)]^{m+1}}{cV(m+1)} \right)$$

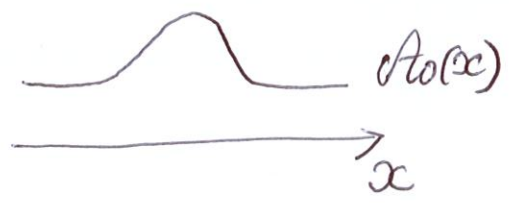
one can see this eq as an implicit equation for the quantity $A = A(x, t)$.
 In this eq. one writes $A_0(x) = A(x, t) - cVt$ and then:

$$A = cVt + A_0 \left(x + \frac{(A - cVt)^{m+1} - A^{m+1}}{cV(m+1)} \right)$$

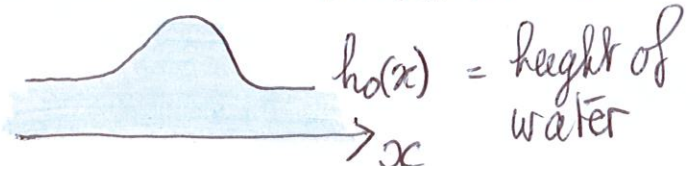
← implicitly defines $A = A(x, t)$

in the case $cV = 0$, one takes the limit $cV \rightarrow 0$ in the above eq. and this simply leads to $A = A_0(x - A^m t)$ as expected.
 implicitly defines A as a fct of (x, t)

Let's consider the case:



which is equivalent, in a river of cross-section and constant breadth to:



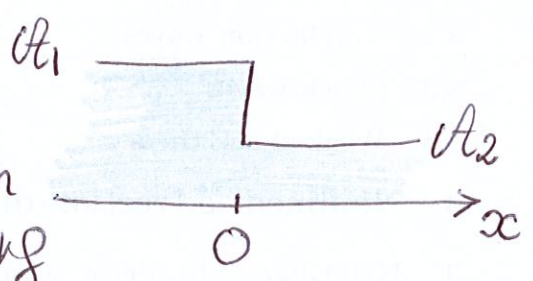
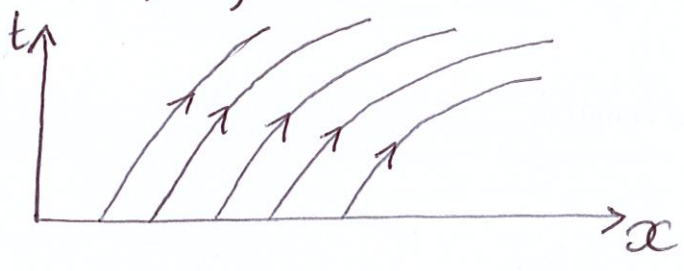
before dealing with this complicated structure let's

first consider the constant initial flow: $t=0$ $\xrightarrow{\quad} \quad \rightarrow x$

This clearly leads to = $\frac{a_1 + \gamma a_1 t}{\gamma a_1 t}$ $\xrightarrow{\quad} \quad \rightarrow x$

and the eq. of a characteristics is = $\left\{ \begin{aligned} x(\tau) &= \frac{[\gamma a_1 \tau + a_1]^{m+1} - a_1^{m+1}}{\gamma a_1 (m+1)} + \bar{x} \\ &\approx a_1^m \tau + \bar{x} \quad \text{for small } \tau \end{aligned} \right.$

The characteristics behave as (remember $m > 0$)



* If one considers the initial condition one will certainly have a shock forming immediately.

A simple analysis of the conservation eq: $\frac{dN}{dt} = \int_{x_1}^{x_2} A_t dx = Q(x_1, t) - Q(x_2, t) + \int_{x_1}^{x_2} \gamma A dx$
 shows (by taking $x_1 < s(t) < x_2$)
 coordinate of the shock

that = $\frac{ds}{dt} = \frac{Q_R - Q_L}{A_R - A_L}$ where $A_R = \lim_{x \rightarrow s(t)} A(x, t)$ (idem for Q)
 $A_L = \lim_{x \rightarrow s^+(t)} A(x, t)$

γA does not appear in this equation.

This gives here $\frac{ds}{dt} = \frac{(a_1 + \gamma a_1 t)^{m+1} - (a_2 + \gamma a_1 t)^{m+1}}{(\gamma a_1 t)^{m+1} - (\gamma a_1 t)^{m+1}} > 0$. Then the characteristics are =

at large t

$\frac{ds}{dt} \approx (m+1)(\gamma a_1 t)^m$

